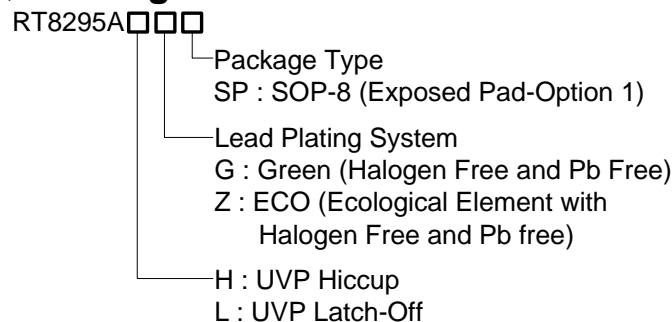


## 2A, 23V, 340kHz Synchronous Step-Down Converter

### General Description

The RT8295A is a high efficiency, monolithic synchronous step-down DC/DC converter that can deliver up to 2A output current from a 4.5V to 23V input supply. The RT8295A's current mode architecture and external compensation allow the transient response to be optimized over a wide range of loads and output capacitors. Cycle-by-cycle current limit provides protection against shorted outputs and soft-start eliminates input current surge during start-up. The RT8295A also provides under voltage protection and thermal shutdown protection. The low current (<3μA) shutdown mode provides output disconnection, enabling easy power management in battery-powered systems. The RT8295A is available in a SOP-8 (Exposed Pad) package.

### Ordering Information



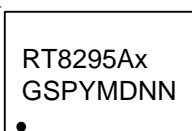
Note :

Richtek products are :

- ▶ RoHS compliant and compatible with the current requirements of IPC/JEDEC J-STD-020.
- ▶ Suitable for use in SnPb or Pb-free soldering processes.

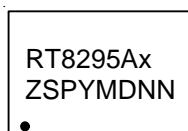
### Marking Information

RT8295AxGSP



RT8295AxGSP : Product Number  
x : H or L  
YMDNN : Date Code

RT8295AxZSP



RT8295AxZSP : Product Number  
x : H or L  
YMDNN : Date Code

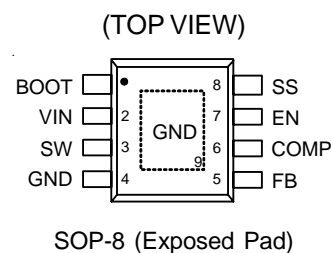
### Features

- ±1.5% High Accuracy Feedback Voltage
- 4.5V to 23V Input Voltage Range
- 2A Output Current
- Integrated N-MOSFET Switches
- Current Mode Control
- Fixed Frequency Operation : 340kHz
- Adjustable Output from 0.8V to 20V
- Up to 95% Efficiency
- Programmable Soft-Start
- Stable with Low-ESR Ceramic Output Capacitors
- Cycle-by-Cycle Over Current Protection
- Input Under Voltage Lockout
- Output Under Voltage Protection
- Thermal Shutdown Protection
- RoHS Compliant and Halogen Free

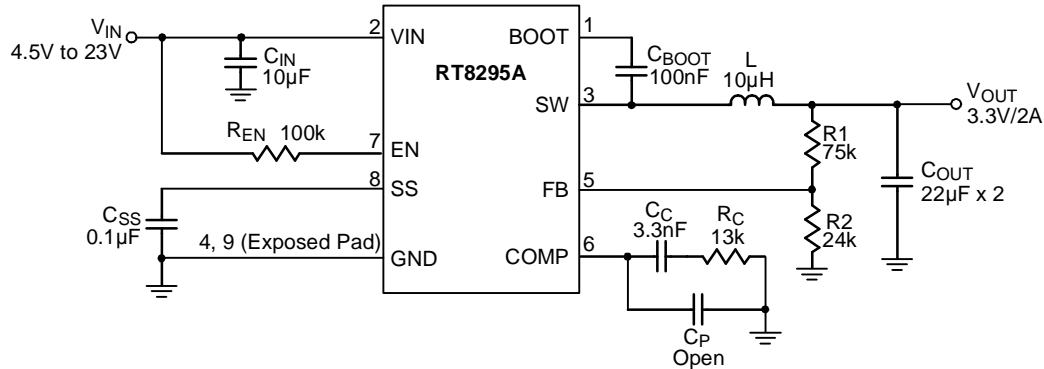
### Applications

- Wireless AP/Router
- Set-Top-Box
- Industrial and Commercial Low Power Systems
- LCD Monitors and TVs
- Green Electronics/Appliances
- Point of Load Regulation of High-Performance DSPs

### Pin Configurations



## Typical Application Circuit



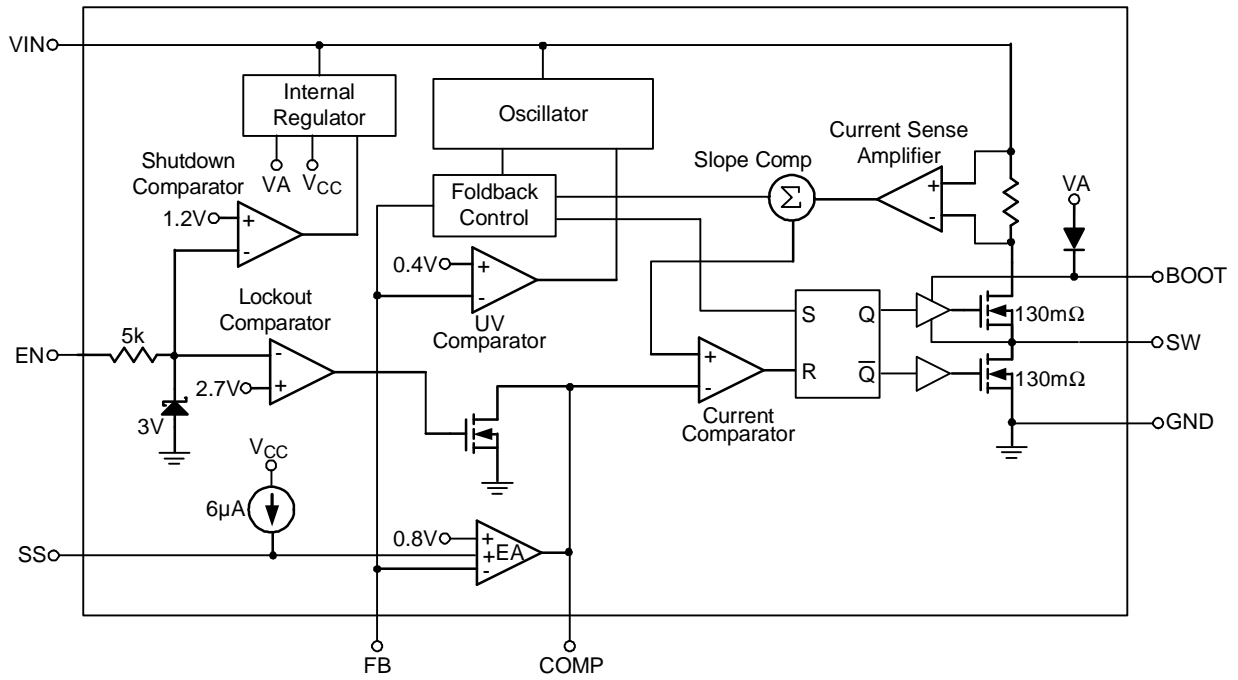
**Table 1. Recommended Component Selection**

V <sub>OUT</sub> (V)	R <sub>1</sub> (kW)	R <sub>2</sub> (kW)	R <sub>C</sub> (kW)	C <sub>C</sub> (nF)	L (mH)	C <sub>OUT</sub> (µF)
8	27	3	27	3.3	22	22 x 2
5	62	11.8	20	3.3	15	22 x 2
3.3	75	24	13	3.3	10	22 x 2
2.5	25.5	12	9.1	3.3	6.8	22 x 2
1.5	10.5	12	4.7	3.3	3.6	22 x 2
1.2	12	24	3.6	3.3	3.6	22 x 2
1	3	12	3	3.3	2	22 x 2

## Functional Pin Description

Pin No.	Pin Name	Pin Function
1	BOOT	Bootstrap for high side gate driver. Connect a 0.1µF or greater ceramic capacitor from BOOT to SW pins.
2	VIN	Input Supply Voltage, 4.5V to 23V. Must bypass with a suitably large ceramic capacitor.
3	SW	Phase Node. Connect this pin to an external L-C filter.
4, 9 (Exposed Pad)	GND	Ground. The exposed pad must be soldered to a large PCB and connected to GND for maximum power dissipation.
5	FB	Feedback Input. This pin is connected to the converter output. It is used to set the output of the converter to regulate to the desired value via an internal resistive voltage divider. For an adjustable output, an external resistive voltage divider is connected to this pin.
6	COMP	Compensation Node. COMP is used to compensate the regulation control loop. Connect a series RC network from COMP to GND. In some cases, an additional capacitor from COMP to GND is required.
7	EN	Chip Enable (Active High). A logic high enables the converter; a logic low forces the RT8295A into shutdown mode reducing the supply current to less than 3µA. Attach this pin to VIN with a 100kΩ pull up resistor for automatic startup.
8	SS	Soft-Start Control Input. SS controls the soft-start period. Connect a capacitor from SS to GND to set the soft-start period. A 0.1µF capacitor sets the soft-start period to 13.5ms.

**Function Block Diagram**



## Absolute Maximum Ratings (Note 1)

Supply Voltage, $V_{IN}$ -----	-0.3V to 25V
Input Voltage, SW -----	-0.3V to ( $V_{IN} + 0.3V$ )
$V_{BOOT} - V_{SW}$ -----	-0.3V to 6V
All Other Pin Voltages -----	-0.3V to 6V
Power Dissipation, $P_D$ @ $T_A = 25^\circ C$	
SOP-8 (Exposed Pad) -----	1.333W
Package Thermal Resistance (Note 2)	
SOP-8 (Exposed Pad), $\theta_{JA}$ -----	75°C/W
SOP-8 (Exposed Pad), $\theta_{JC}$ -----	15°C/W
Lead Temperature (Soldering, 10 sec.) -----	260°C
Junction Temperature -----	150°C
Storage Temperature Range -----	-65°C to 150°C
ESD Susceptibility (Note 3)	
HBM (Human Body Mode) -----	2kV
MM (Machine Mode) -----	200V

## Recommended Operating Conditions (Note 4)

Supply Voltage, $V_{IN}$ -----	4.5V to 23V
Junction Temperature Range -----	-40°C to 125°C
Ambient Temperature Range -----	-40°C to 85°C

## Electrical Characteristics

( $V_{IN} = 12V$ ,  $T_A = 25^\circ C$ , unless otherwise specified)

Parameter	Symbol	Test Conditions	Min	Typ	Max	Unit
Shutdown Supply Current		$V_{EN} = 0V$	--	0.5	3	$\mu A$
Supply Current		$V_{EN} = 3V$ , $V_{FB} = 0.9V$	--	0.8	1.2	mA
Feedback Voltage	$V_{FB}$	$4.5V \leq V_{IN} \leq 23V$	0.788	0.8	0.812	V
Error Amplifier Transconductance	$G_{EA}$	$\Delta IC = \pm 10\mu A$	--	940	--	$\mu A/V$
High Side Switch On Resistance	$R_{DS(ON)1}$		--	130	--	m $\Omega$
Low Side Switch On-Resistance	$R_{DS(ON)2}$		--	130	--	m $\Omega$
High Side Switch Leakage Current		$V_{EN} = 0V$ , $V_{SW} = 0V$	--	0	10	$\mu A$
Upper Switch Current Limit		Min. Duty Cycle, $V_{BOOT} - V_{SW} = 4.8V$	--	4.3	--	A
COMP to Current Sense Transconductance	$G_{CS}$		--	4	--	A/V
Oscillation Frequency	$f_{OSC1}$		300	340	380	kHz
Short Circuit Oscillation Frequency	$f_{OSC2}$	$V_{FB} = 0V$	--	100	--	kHz
Maximum Duty Cycle	$D_{MAX}$	$V_{FB} = 0.7V$	--	93	--	%
Minimum On Time	$t_{ON}$		--	100	--	ns

*To be continued*

Parameter		Symbol	Test Conditions	Min	Typ	Max	Unit
EN Input Threshold Voltage	Logic-High	$V_{IH}$		2.7	--	5.5	V
	Logic-Low	$V_{IL}$		--	--	0.4	
Input Under Voltage Lockout Threshold		$V_{UVLO}$	$V_{IN}$ Rising	3.8	4.2	4.5	V
Input Under Voltage Lockout Hysteresis		$\Delta V_{UVLO}$		--	320	--	mV
Soft-Start Current		$I_{SS}$	$V_{SS} = 0V$	--	6	--	$\mu A$
Soft-Start Period		$t_{SS}$	$C_{SS} = 0.1\mu F$	--	13.5	--	ms
Thermal Shutdown		$T_{SD}$		--	150	--	$^{\circ}C$

**Note 1.** Stresses listed as the above "Absolute Maximum Ratings" may cause permanent damage to the device. These are for stress ratings. Functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions for extended periods may remain possibility to affect device reliability.

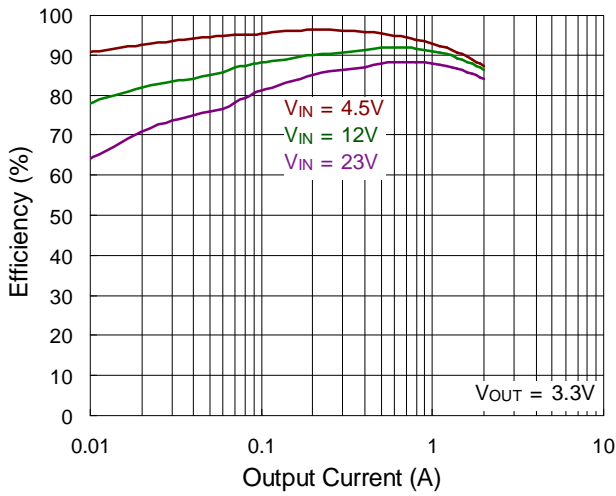
**Note 2.**  $\theta_{JA}$  is measured in natural convection at  $T_A = 25^{\circ}C$  on a high effective thermal conductivity four-layer test board of JEDEC 51-7 thermal measurement standard. The measurement case position of  $\theta_{JC}$  is on the exposed pad of the package.

**Note 3.** Devices are ESD sensitive. Handling precaution is recommended.

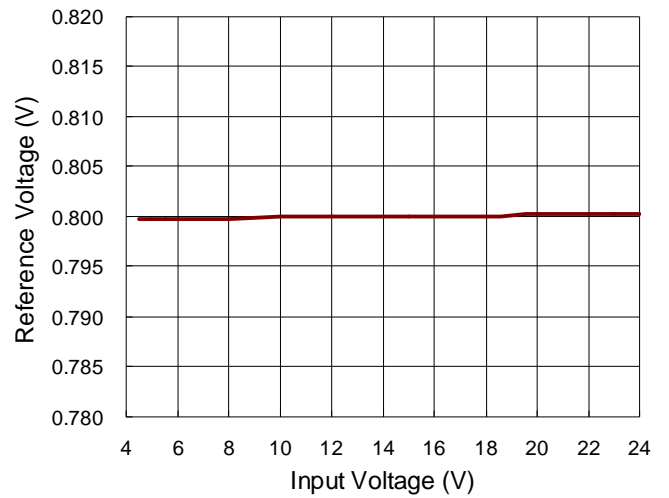
**Note 4.** The device is not guaranteed to function outside its operating conditions.

## Typical Operating Characteristics

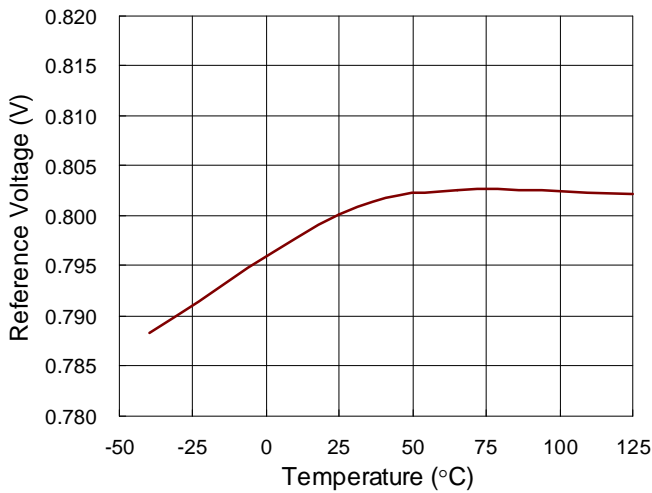
**Efficiency vs. Output Current**



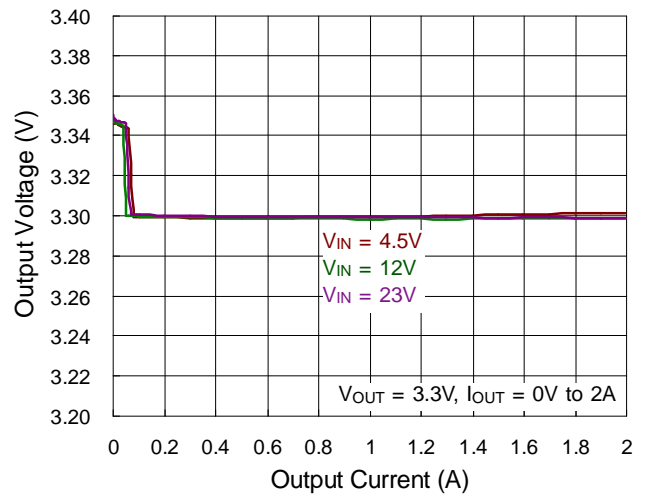
**Reference Voltage vs. Input Voltage**



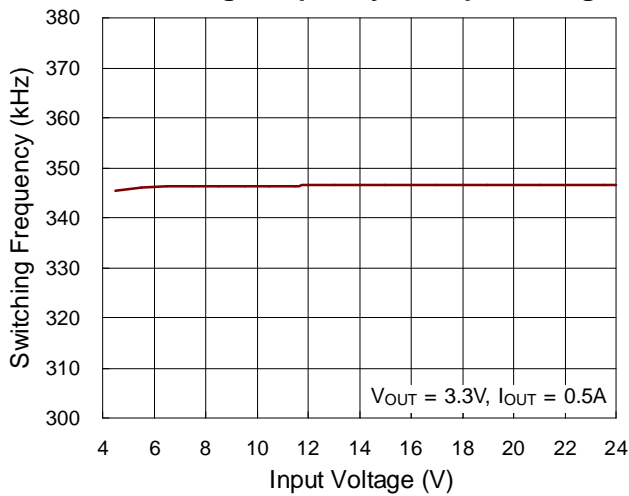
**Reference Voltage vs. Temperature**



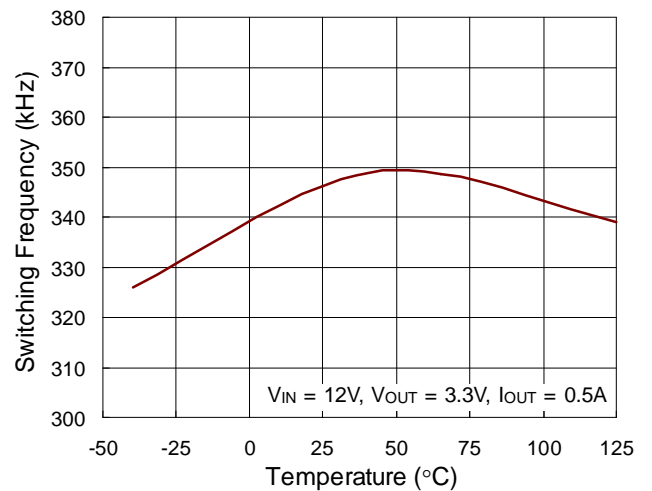
**Output Voltage vs. Output Current**



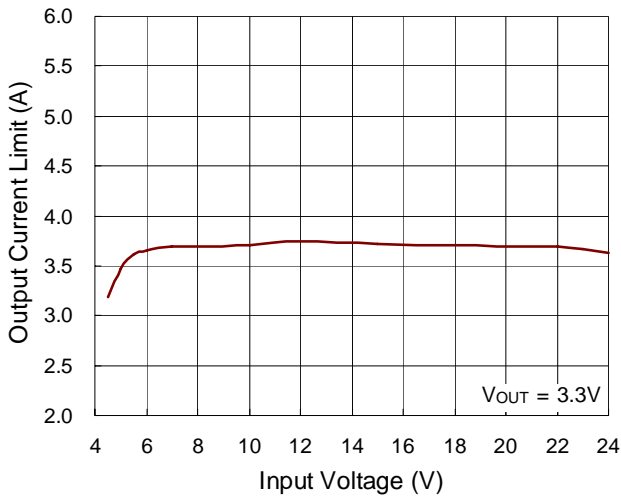
**Switching Frequency vs. Input Voltage**



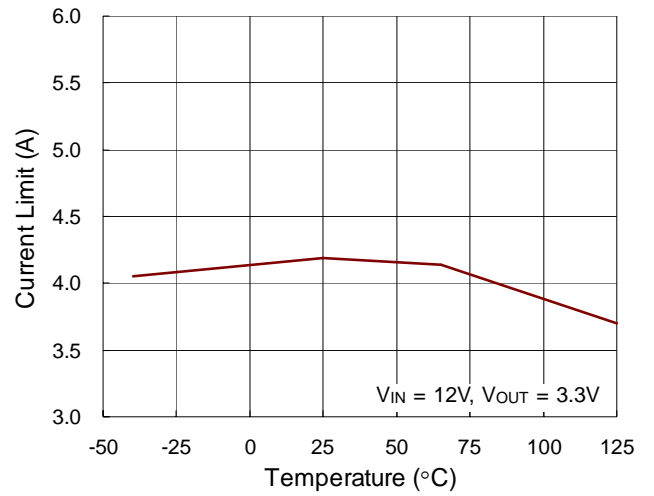
**Switching Frequency vs. Temperature**



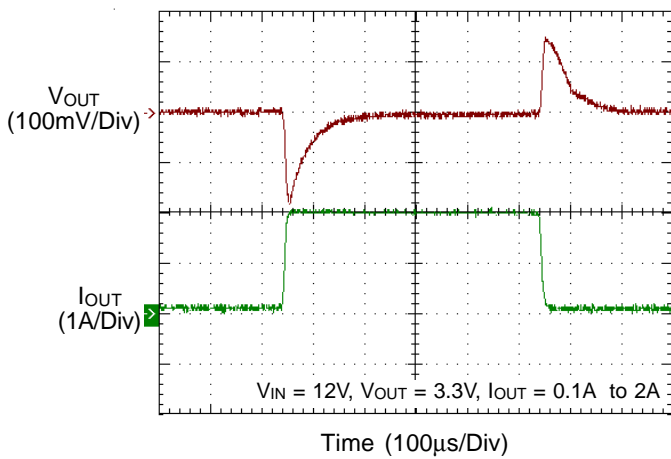
**Output Current Limit vs. Input Voltage**



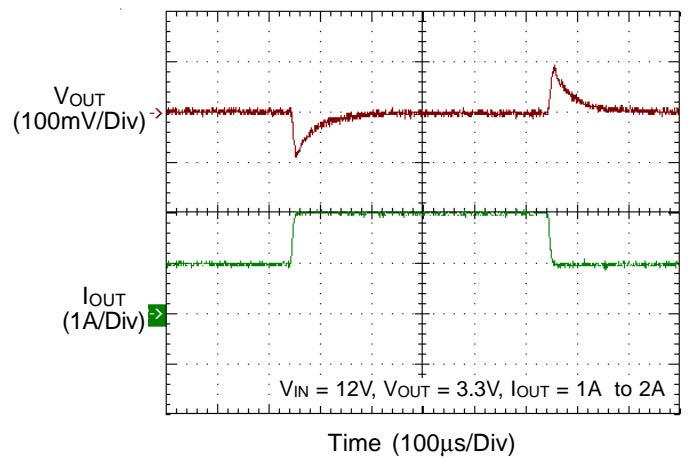
**Current Limit vs. Temperature**



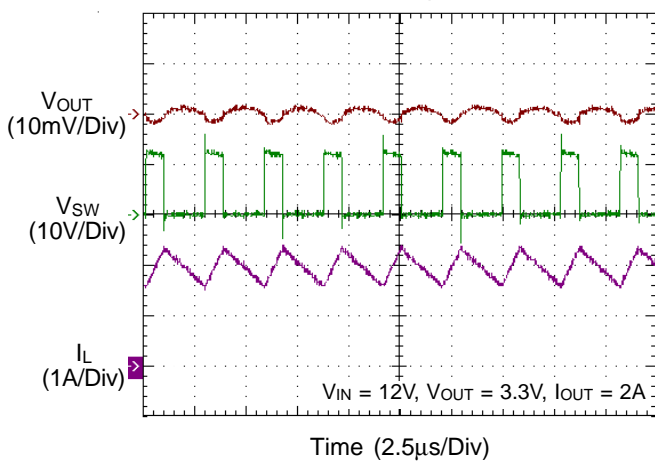
**Load Transient Response**



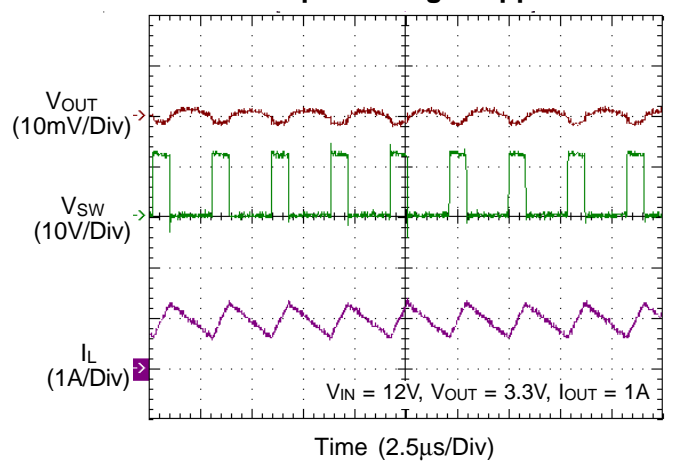
**Load Transient Response**



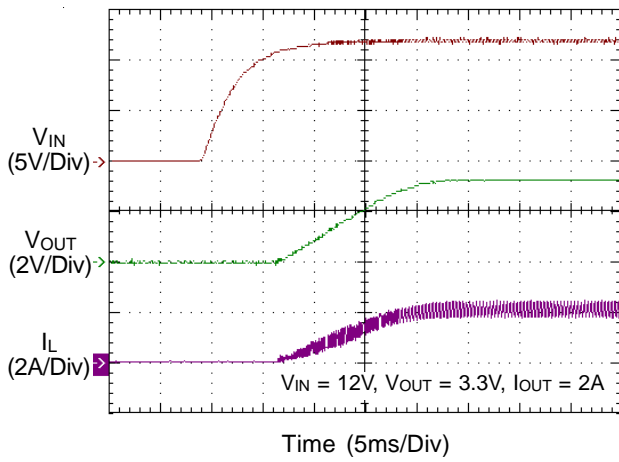
**Output Voltage Ripple**



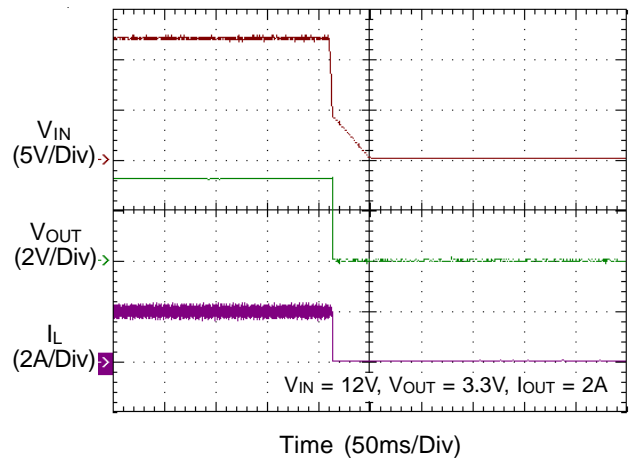
**Output Voltage Ripple**



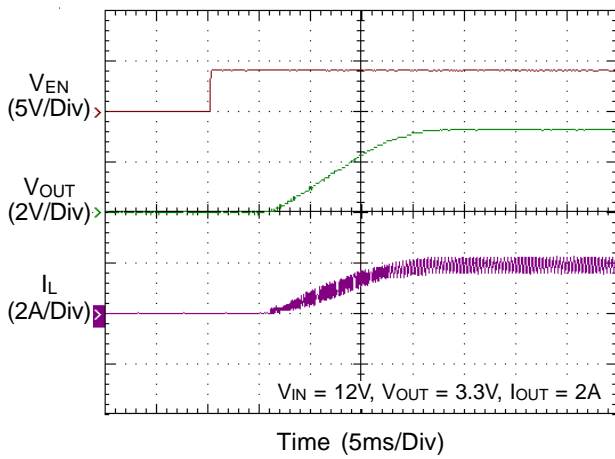
Power On from V<sub>IN</sub>



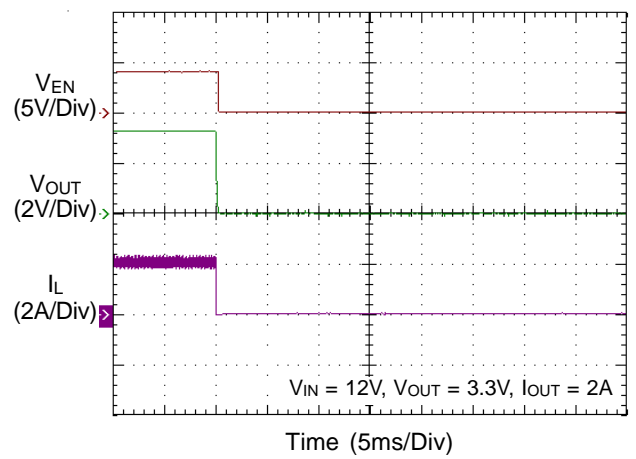
Power Off from V<sub>IN</sub>



Power On from EN



Power Off from EN









response as described in a later section.

The output ripple,  $\Delta V_{OUT}$ , is determined by :

$$\Delta V_{OUT} \leq \Delta I_L \left[ ESR + \frac{1}{8fC_{OUT}} \right]$$

The output ripple will be highest at the maximum input voltage since  $\Delta I_L$  increases with input voltage. Multiple capacitors placed in parallel may be needed to meet the ESR and RMS current handling requirement. Dry tantalum, special polymer, aluminum electrolytic and ceramic capacitors are all available in surface mount packages. Special polymer capacitors offer very low ESR value. However, it provides lower capacitance density than other types. Although Tantalum capacitors have the highest capacitance density, it is important to only use types that pass the surge test for use in switching power supplies. Aluminum electrolytic capacitors have significantly higher ESR. However, it can be used in cost-sensitive applications for ripple current rating and long term reliability considerations. Ceramic capacitors have excellent low ESR characteristics but can have a high voltage coefficient and audible piezoelectric effects. The high Q of ceramic capacitors with trace inductance can also lead to significant ringing.

Higher values, lower cost ceramic capacitors are now becoming available in smaller case sizes. Their high ripple current, high voltage rating and low ESR make them ideal for switching regulator applications. However, care must be taken when these capacitors are used at input and output. When a ceramic capacitor is used at the input and the power is supplied by a wall adapter through long wires, a load step at the output can induce ringing at the

input,  $V_{IN}$ . At best, this ringing can couple to the output and be mistaken as loop instability. At worst, a sudden inrush of current through the long wires can potentially cause a voltage spike at  $V_{IN}$  large enough to damage the part.

**Checking Transient Response**

The regulator loop response can be checked by looking at the load transient response. Switching regulators take several cycles to respond to a step in load current. When a load step occurs,  $V_{OUT}$  immediately shifts by an amount equal to  $\Delta I_{LOAD} (ESR)$  and  $C_{OUT}$  also begins to be charged or discharged to generate a feedback error signal for the regulator to return  $V_{OUT}$  to its steady-state value. During this recovery time,  $V_{OUT}$  can be monitored for overshoot or ringing that would indicate a stability problem.

**EMI Consideration**

Since parasitic inductance and capacitance effects in PCB circuitry would cause a spike voltage on SW pin when high side MOSFET is turned-on/off, this spike voltage on SW may impact on EMI performance in the system. In order to enhance EMI performance, there are two methods to suppress the spike voltage. One way is by placing an R-C snubber between SW and GND and locating them as close as possible to the SW pin (see Figure 5). Another method is by adding a resistor in series with the bootstrap capacitor,  $C_{BOOT}$ , but this method will decrease the driving capability to the high side MOSFET. It is strongly recommended to reserve the R-C snubber during PCB layout for EMI improvement. Moreover, reducing the SW trace area and keeping the main power in a small loop will be helpful on EMI performance. For detailed PCB layout guide, please refer to the section Layout Considerations.

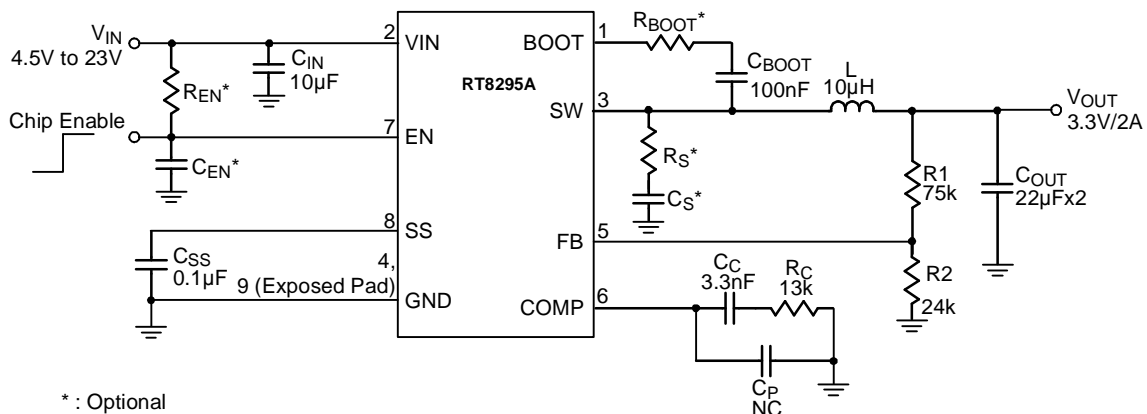


Figure 5. Reference Circuit with Snubber and Enable Timing Control

## Thermal Considerations

For continuous operation, do not exceed the maximum operation junction temperature 125°C. The maximum power dissipation depends on the thermal resistance of IC package, PCB layout, the rate of surroundings airflow and temperature difference between junction to ambient. The maximum power dissipation can be calculated by following formula :

$$P_{D(MAX)} = (T_{J(MAX)} - T_A) / \theta_{JA}$$

where  $T_{J(MAX)}$  is the maximum operation junction temperature,  $T_A$  is the ambient temperature and the  $\theta_{JA}$  is the junction to ambient thermal resistance.

For recommended operating conditions specification of RT8295A, the maximum junction temperature is 125°C. The junction to ambient thermal resistance  $\theta_{JA}$  is layout dependent. For SOP-8(Exposed Pad) package, the thermal resistance  $\theta_{JA}$  is 75°C/W on the standard JEDEC 51-7 four-layers thermal test board. The maximum power dissipation at  $T_A = 25^\circ\text{C}$  can be calculated by following formula :

$$P_{D(MAX)} = (125^\circ\text{C} - 25^\circ\text{C}) / (75^\circ\text{C/W}) = 1.333\text{W}$$

(min.copper area PCB layout)

$$P_{D(MAX)} = (125^\circ\text{C} - 25^\circ\text{C}) / (49^\circ\text{C/W}) = 2.04\text{W}$$

(70mm<sup>2</sup> copper area PCB layout)

The thermal resistance  $\theta_{JA}$  of SOP-8 (Exposed Pad) is determined by the package architecture design and the PCB layout design. However, the package architecture design had been designed. If possible, it's useful to increase thermal performance by the PCB layout copper design. The thermal resistance  $\theta_{JA}$  can be decreased by adding copper area under the exposed pad of SOP-8 (Exposed Pad) package.

As shown in Figure 6, the amount of copper area to which the SOP-8 (Exposed Pad) is mounted affects thermal performance. When mounted to the standard SOP-8 (Exposed Pad) pad (Figure 6.a),  $\theta_{JA}$  is 75°C/W. Adding copper area of pad under the SOP-8 (Exposed Pad) (Figure 6.b) reduces the  $\theta_{JA}$  to 64°C/W. Even further increasing the copper area of pad to 70mm<sup>2</sup> (Figure 6.e) reduces the  $\theta_{JA}$  to 49°C/W.

The maximum power dissipation depends on operating ambient temperature for fixed  $T_{J(MAX)}$  and thermal resistance  $\theta_{JA}$ . For RT8295A package, the derating curves in Figure 7 allow the designer to see the effect of rising ambient temperature on the maximum power dissipation .

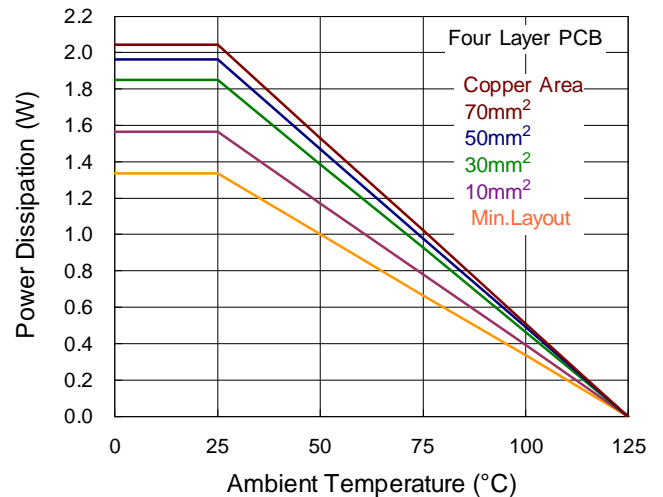
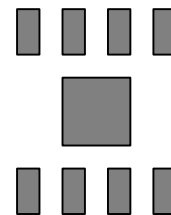
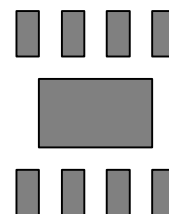


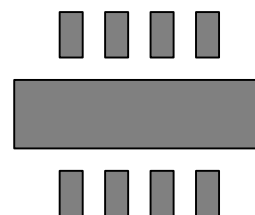
Figure 7. Derating Curves for RT8295A Package



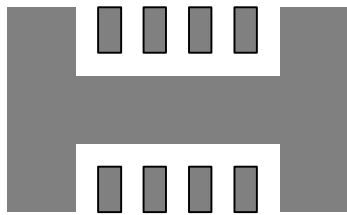
(a) Copper Area = (2.3 x 2.3) mm<sup>2</sup>,  $\theta_{JA} = 75^\circ\text{C/W}$



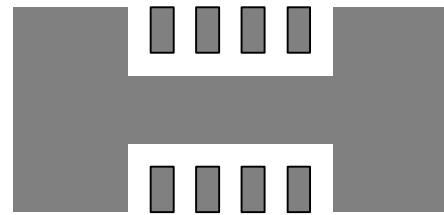
(b) Copper Area = 10mm<sup>2</sup>,  $\theta_{JA} = 64^\circ\text{C/W}$



(c) Copper Area = 30mm<sup>2</sup>,  $\theta_{JA} = 54^\circ\text{C/W}$



(d) Copper Area = 50mm<sup>2</sup>,  $\theta_{JA} = 51^{\circ}\text{C/W}$



(e) Copper Area = 70mm<sup>2</sup>,  $\theta_{JA} = 49^{\circ}\text{C/W}$

Figure 6. Thermal Resistance vs. Copper Area Layout Design

**Layout Considerations**

For best performance of the RT8295A, the following layout guidelines must be strictly followed.

- } Input capacitor must be placed as close to the IC as possible.
- } SW should be connected to inductor by wide and short trace. Keep sensitive components away from this trace.
- } The feedback components must be connected as close to the device as possible

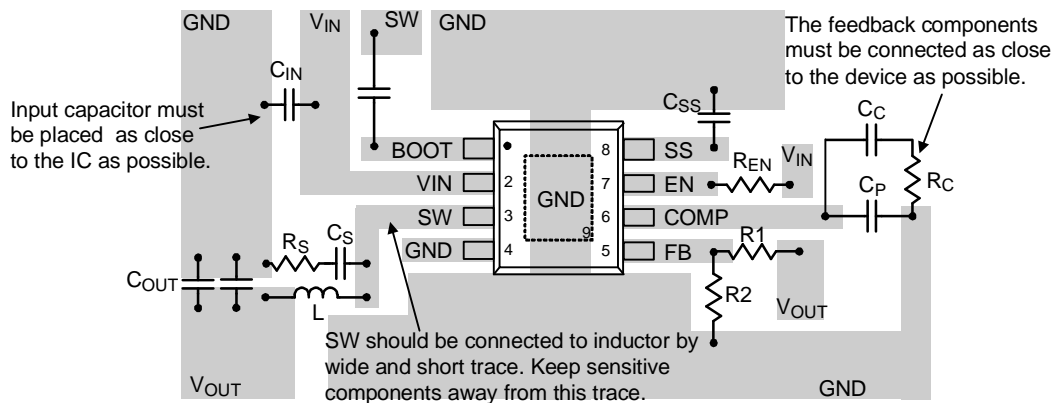
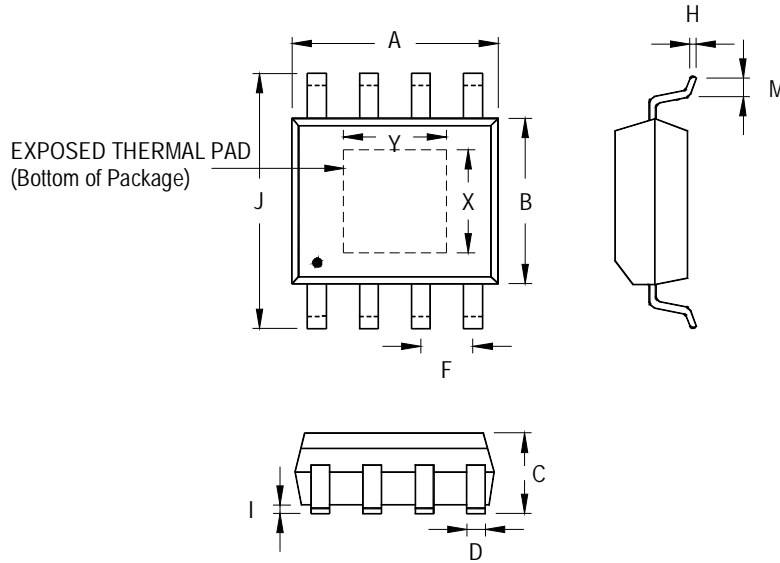


Figure 8. PCB Layout Guide

**Table 3. Suggested Capacitors for C<sub>IN</sub> and C<sub>OUT</sub>**

Location	Component Supplier	Part No.	Capacitance (mF)	Case Size
C <sub>IN</sub>	MURATA	GRM31CR61E106K	10	1206
C <sub>IN</sub>	TDK	C3225X5R1E106K	10	1206
C <sub>IN</sub>	TAIYO YUDEN	TMK316BJ106ML	10	1206
C <sub>OUT</sub>	MURATA	GRM31CR60J476M	47	1206
C <sub>OUT</sub>	TDK	C3225X5R0J476M	47	1210
C <sub>OUT</sub>	MURATA	GRM32ER71C226M	22	1210
C <sub>OUT</sub>	TDK	C3225X5R1C22M	22	1210

Outline Dimension



Symbol	Dimensions In Millimeters		Dimensions In Inches		
	Min	Max	Min	Max	
A	4.801	5.004	0.189	0.197	
B	3.810	4.000	0.150	0.157	
C	1.346	1.753	0.053	0.069	
D	0.330	0.510	0.013	0.020	
F	1.194	1.346	0.047	0.053	
H	0.170	0.254	0.007	0.010	
I	0.000	0.152	0.000	0.006	
J	5.791	6.200	0.228	0.244	
M	0.406	1.270	0.016	0.050	
Option 1	X	2.000	2.300	0.079	0.091
	Y	2.000	2.300	0.079	0.091
Option 2	X	2.100	2.500	0.083	0.098
	Y	3.000	3.500	0.118	0.138

8-Lead SOP (Exposed Pad) Plastic Package

**Richtek Technology Corporation**

Headquarter  
 5F, No. 20, Taiyuen Street, Chupei City  
 Hsinchu, Taiwan, R.O.C.  
 Tel: (8863)5526789 Fax: (8863)5526611

**Richtek Technology Corporation**

Taipei Office (Marketing)  
 5F, No. 95, Minchiuan Road, Hsintien City  
 Taipei County, Taiwan, R.O.C.  
 Tel: (8862)86672399 Fax: (8862)86672377  
 Email: marketing@richtek.com

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